

WAFFLE SLAB- ANALYSIS BY DIFFERENT METHODS

Naziya Ghanchi¹, Chitra V.²

¹ P.G. student, Lecturer, Civil Engineering Department, Saraswati College of Engineering, Maharashtra, India,
ghanchi.naziya23@gmail.com

² Asst. Professors, Civil Engineering Department, Saraswati College of Engineering, Maharashtra, India,
Itzchitra.v@gmail.com

ABSTRACT:

There are various approaches available for analyzing the waffle slab system. In present study some of these approaches are studied and compared with each other. The comparison is done on the basis of flexural parameters such as bending moments and shear forces obtained from various methods. For carrying out study, halls having constant width 10.00m and varying ratio of hall dimensions (L/B) from 1 to 1.5 are considered.

KEYWORDS: Waffle Slab, Plate theory, Rankine-Grashoff method, Stiffness method.

I. INTRODUCTION

Waffle slabs structure are defined as a combinations of a flat flange plate, or deck, and a system of equally spaced parallel ribs, or grillage, that may be arranged in either orthogonal or skew assembly with monolithic inter-sections. They are also known as two way ribbed flat slab and it includes recesses between the ribs.

Waffle slabs have economical and constructional benefits. They are used for heavy loads and large spans structures as they exhibit higher stiffness and smaller deflection. As a result, waffle slabs has been widely used for office buildings ,hotels, auditoriums, vestibules, theatre halls, show rooms of shops where column free space is often the main requirement.

Dimensions Considered For the comparison purpose, the width of the hall is kept constant as 10.00 m and length is increased by an interval of



Fig 1: Typical waffle slab floor

II. METHODS OF ANALYSIS

Various approaches available for the analysis of waffle slab from which few are as listed below.

- 1) Analysis of grid by Rankine – Grashoff method.
- 2) Analysis by plate theory.
- 3) Stiffness method.

2.1 Rankine - Grashoff Method

This is an approximate method. It is based on equating deflections in either direction at the

junctions of ribs. This method is suitable for small span grids with the spacing of ribs not exceeding 1.50 m. In this method the slab is considered as simply supported on edges. (Refer Figure. No.2) This method computes moments and shear force per unit width of slab strip.

2.2 Plate Analogy Method

This is a rigorous method of analysis. This is based on Timoshenko's analysis of orthotropic plate theory considering plane stress analysis. As in Rankine-Grashoff method, in this method also the analysis is done by considering the grid simply supported on edges (Refer Fig. No.2).

Bending & torsion moments and shears are obtained per unit width of slab strip.

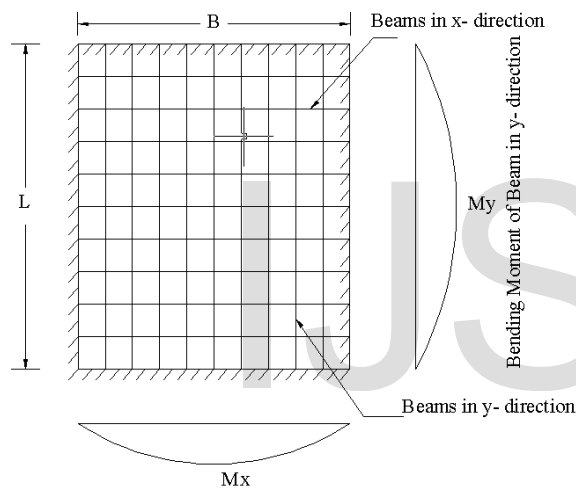


Figure No. 2 Typical grid considered in Rankine-Grashoff and Plate theory (Below grid)

2.3 Stiffness Method This method is based on matrix formulation of the stiffness of the structure and gives closed form solution. By using this method the analysis can be done by considering rigid supports as well. Various application software's are available to carry out analysis by this method. In the present work while analyzing waffle floor frame by stiffness method, the simple supports are considered at closer distance so as to simulate the support conditions similar to Rankine-Grashoff method and Plate theory. (Refer Fig. No.3).

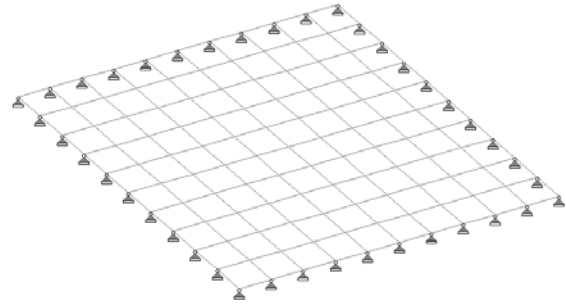


Figure No. 3 Typical Grid floor considered in stiffness method.

III. THEORETICAL FORMULATION

3.1 Typical Geometrical Data for L/B=1.0

Width of Hall (a) = 10.00 m, Length of Hall (b) = 10.00 m
Spacing of grids in x-direction (a1) and y-direction (b1) = 1.00 m
Thickness of slab (Df) = 0.1 m
Width of ribs (bw) = 0.23 m

3.2 Load Calculations

The loads on floor slab are calculated on the basis of Density of reinforced concrete and floor finish considered as 25kN/m².
Live load intensity=5 kN/m²
Total dead load of floor area (10.00 m x 10.00 m) =730.180 kN
Total live load on floor area (10.00 m x 10.00 m) =500 kN

IV. RESULT DISCUSSION

The results of the analysis carried by Rankine-Grashoff method, Plate theory, and Stiffness method are presented below.

Analysis by Rankine-Grashoff method and Plate theory manual calculation is done. The analysis by Stiffness method is carried out using STAAD.pro, application software.

After analyzing such grids by above discussed three methods, the results are presented here

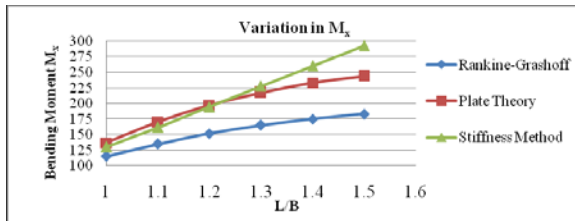


Figure no. 4 comparison of maximum bending moments for beams in x-direction (M_x)

The Figure No.4 shows the variations in maximum bending moment (M_x) for the beams which are running in x- direction for various (L/B) ratios by various methods of analysis. The graph shows that the bending moment (M_x) is increasing with increasing L/B ratio. The nature of bending moment variation is non-linear for Rankine-Grashoff method and Plate theory approach. However, using stiffness method bending moment (M_x) is increasing almost linearly with increasing L/B ratio. Up to L/B = 1.3, the bending moment (M_x) is in close proximity for Plate Theory and Stiffness method. With increase in L/B beyond 1.3, the bending moment (M_x) given by Plate theory is lower than those given by the Stiffness method in the range of 5% to 17%. Rankine-Grashoff method estimates lowest values of M_x , amongst all above three methods.

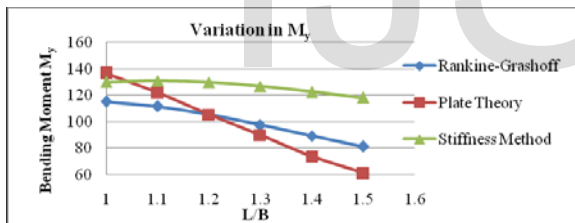


Figure no. 5 comparison of maximum bending moments for beams in y-direction (M_y)

The Figure No.5 shows the variations in maximum bending moment (M_y) for the beams which are running in y- direction for various (L/B) ratios by various methods of analysis. The bending moment (M_y) is decreasing as L/B goes on increasing for all three methods. As the L/B ratio increases, the variation is observed to be nonlinear for Rankine-Grashoff method and Stiffness method. However, for Plate theory approach the variation is almost linear. The graph also shows that, the bending moment (M_y) is in close proximity for Plate theory and Stiffness method up to L/B= 1.1. With increase in L/B beyond 1.1, the bending moments (M_y) given by Plate theory is lower than that given by the Stiffness method in the range of 7% to 48%.With

increasing L/B ratio these values become lower for plate theory.

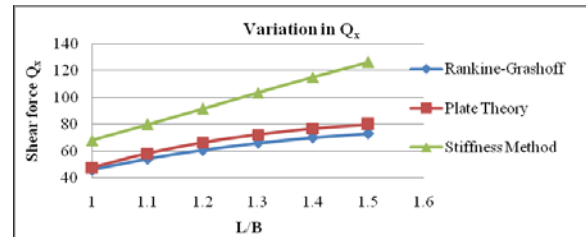


Figure no. 6 comparison of maximum shear force for beams in x-direction (Q_x)

The Figure No.6 shows the variations in maximum Shear Force (Q_x) for the beams which are running in x- direction for various (L/B) ratios by various methods of analysis. The variation of shear force (Q_x) is observed to be nonlinear for Rankine-Grashoff method and Plate theory. However, for stiffness method the variation of shear force (Q_x) is almost linear. Rankine-Grashoff method estimates lowest values of shear force (Q_x) amongst above three methods. For a given L/B ratio, the Stiffness method shows highest value of shear force (Q_x), than that is shown by Plate theory and Rankine-Grashoff method. Plate theory shows less value of shear force (Q_x) by 30% to 37% than the Stiffness method for L/B = 1 to 1.5

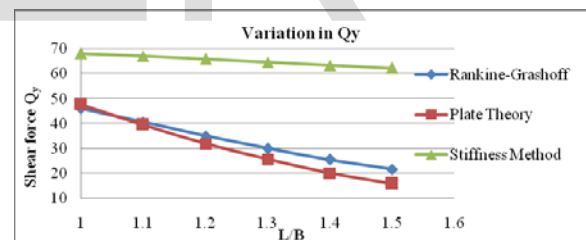


Figure no. 7 comparison of maximum shear force for beams in y-direction (q_y)

The Figure No.7 shows the variations in maximum Shear Force (Q_y) for the beams which are running in y- direction for various (L/B) ratios by various methods of analysis. The graph shows that shear force (Q_y) is decreasing almost linearly with increasing L/B ratio, for all the three methods.

The stiffness method shows highest value of shear force (Q_y) for the given L/B ratio. Rankine-Grashoff method shows lower values in the range of 32% to 60% for L/B= 1 to 1.5 than that of stiffness method. Plate theory shows values lower by 30% to 68% for L/B =1 to 1.5.

V. CONCLUSION

1) Rankine-Grashoff method is an approximate method. Rankine-Grashoff method does not give the values of torsion moments. Rankine-Grashoff method underestimates critical bending moment (M_x) and shear force (Q_x).

2) Plate theory and Rankine-Grashoff method are used for simple support conditions. On the contrary the stiffness method can be used for rigid supports as well.

3) In Plate theory and Rankine-Grashoff method, design moments and shear force in Peripheral beams cannot be obtained. In fact in monolithic framed construction, design moments and shears in peripheral beams will be the maximum.

4) Initially, up to $L/B=1.2$, Plate theory shows higher value of bending moment (M_x) with respect to stiffness method. With increasing L/B , beyond $L/B=1.3$ Plate theory shows lower value of bending moment (M_x) as compared to stiffness method.

5) Stiffness method shows higher value of shear force (Q_x) as compared to other methods discussed. Plate theory shows less values of Q_x than that of stiffness method.

6) Stiffness method is accurate & more suitable to arrive at design moments and shear force. Also Stiffness method takes less time for analysis.

REFERENCES

[1] A Sathawane, R.S. Deotale, Analysis and Design of Flat Slab and Grid Slab and Their Comparison, International Journal of Engineering Research and Applications Vol. 1, Issue 3, pp.837-848

[2] Ibrahim Vepari, Dr. H.S. Patel, Study on Economical Aspects of Long Span Slabs. 13-14 May 2011 B.V.M. Engineering College, V. V. Nagar, Gujarat, India, National Conference on Recent Trends in Engineering & Technology, 13-14 May 2011

[3] P. F. Schwetz, F. P. S. L. Gastal, L. C. P. Silva F, Numerical and Experimental Study of a Real Scale Waffle Slab, IBRACON Structures and Materials Journal • 2009 • vol. 2, No.4, p. 380 - 403 • ISSN 1983-4195

[4] N. Krishnaraju, Advanced Reinforced concrete design (IS:456-2000) (C B S Publishers and distributors, CBS Plaza, New Delhi, India, 2005)

[5] S. Timoshenko and S. Woinowsky-Krieger Theory of plates and shell (McGraw-Hill Book Company)

[6] S. Timoshenko and J. N. Goodier Theory of Elasticity (McGraw-Hill Book Company, 1951)

[7] Charles E Reynolds and James C. Steedman, Reinforced Concrete Designer's Handbook (E and F N Spon Taylor and Francis Group, 1988)

[8] IS: 456, "Code of practice for plain and R.C. Structures", (Bureau of Indian Standards, New Delhi. 2000)

[9] I.S.875 Part-I, Part-II (Bureau of Indian Standards, New Delhi,1987)

[10] John J Panak and Hudson Matlock, A Discrete Element Method of Analysis for Orthogonal Slab and Grid Bridge Floor System, (Research No 56-25, Development Methods for Computer Simulation of Beam Columns And Grid Beam And Slab System Research Project 3-5-63-56, Center for Highway Research, The University of Texas At Austin 1972)

[11] Baishali Das Static And Dynamic Analysis Of Grid Beams, Project report for Bachelor of Technology, Department of civil engineering, National Institute of technology, Rourkela 2010